

Space age semaphore operation

Lawrence Boul

HAVING DESIGNED and built the New Zealand Finescale semaphore signal kits, the final challenge was to attach them to an operating device.

The elegance of the McKenzie and Holland semaphore signal was conceived in an age when labour was cheap and the options for mechanical actuation were few. Thus signals were operated manually, via levers, cranks, wires, pulleys and rods. Watching the movement of signals at preserved sites, or on film, reveals the almost lazy action with which the arms move. Not infrequently they bounce on their stops. Attempts to replicate this latter feature have been reported in British journals, but on my portable layout I was primarily interested in replicating a leisurely movement, quietly, and preferably without the expense of a Tortoise or Switch-master point machine per arm.

The features required were:

- low noise
- slow movement
- simplicity
- ease of adjustment
- moderate cost
- robustness.

As a result, I was drawn to the features of shape memory alloys (SMA). These are alloys that change shape with temperature as a result of their intrinsic properties and conditions of manufacture. Heating is easily achieved by passing a current through the article.

The technical requirements for SMA use are given in the sidebar. This information is taken from *Model Railway Journal* number 73 (1994) and Jacques Le Plat's documentation and website (<http://users.skynet.be/pro-rail/>).

I have previously built a number of SMA devices. All have worked to varying degrees, but were less than perfect. My initial attempts were rather too complicated. The current version is far simpler and is ideal for my needs. The drawing and photographs illustrate the design basics. The important features are:

- A flat design, where the essential mechanicals can be achieved in a thickness of around 1.5 mm. This means that it is easy to stack up operating units for a signal with multiple arms. Note that the memory wire terminations in the photos are offset slightly, which simplifies electrical isolation.
- Easily adjustable. The mechanism is set up so that the coupling with the signal is a 0.85 mm external diameter capillary tube. This means that the operating wire can easily be soldered into this without clever measurement, and that adjustment is easily achieved by warming the joint. As the off condition of the

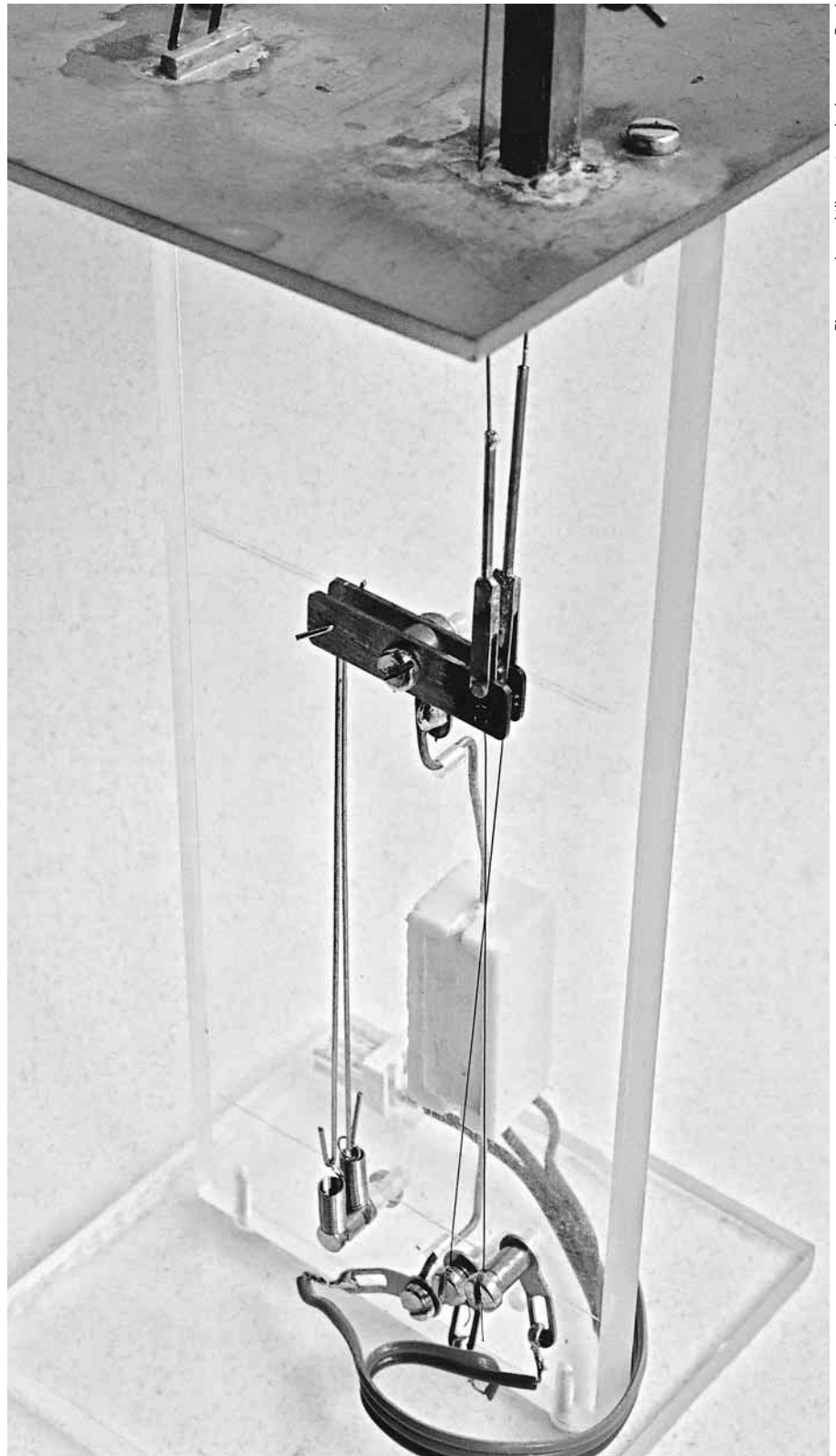
signal corresponds to the cold condition for the SMA, the signal operating rod is soldered within the capillary tube at that state. The total travel depends on the length of the SMA wire. This should be around 60 mm for an NZ Finescale mechanism when set up as shown.

- The SMA is easily replaced in case of damage – though this is reportedly unlikely. I have to say that I have blown a few of these during experiments, but always this has been due to an excess of current due to error on my part. Used properly they should last for a few million cycles, which is probably more than the switch I will use to operate them.
- The SMA is attached without the use of heat (ie solder). At the lever end passing it through three 0.3 mm holes retains it by friction, and at the fixed end a screw between two bushes clamps it.
- Although not an operating requirement, note in the photographs that the base-board-level mounting plate of the signal is quite large, and that the operating unit base is the same size. This enables the signal to be placed on any side during maintenance, without fear of damage, or for the unit to be placed upright without risk of toppling.

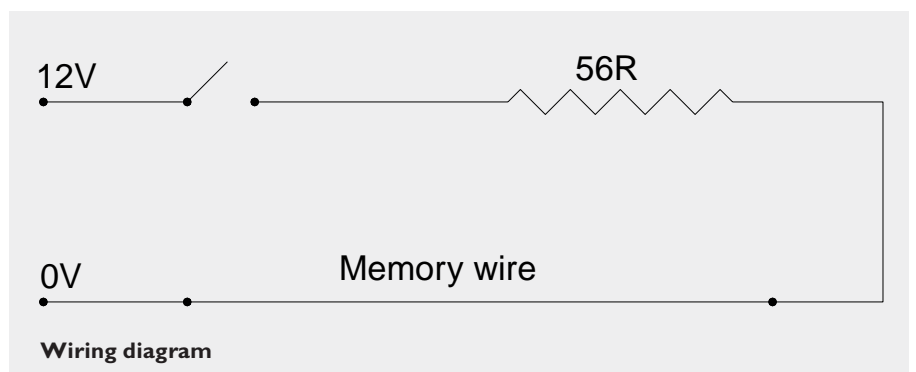
The diagrams show the electrical and physical necessities. I chose a vertically orientated, portable and self-supporting design, because that suits my layout situation. My units are made from clear Perspex as I find it easy to work with, but other materials would be quite suitable. In my units, I have used M2 screws in tapped holes to hold everything together. I have also used turned brass bushes for pivots and wire clamps. These are probably not strictly necessary, but good engineering. The units are very easy to make, requiring simple assembly of simple parts. The trick is in the memory wire – and the hard work there has been done for you.

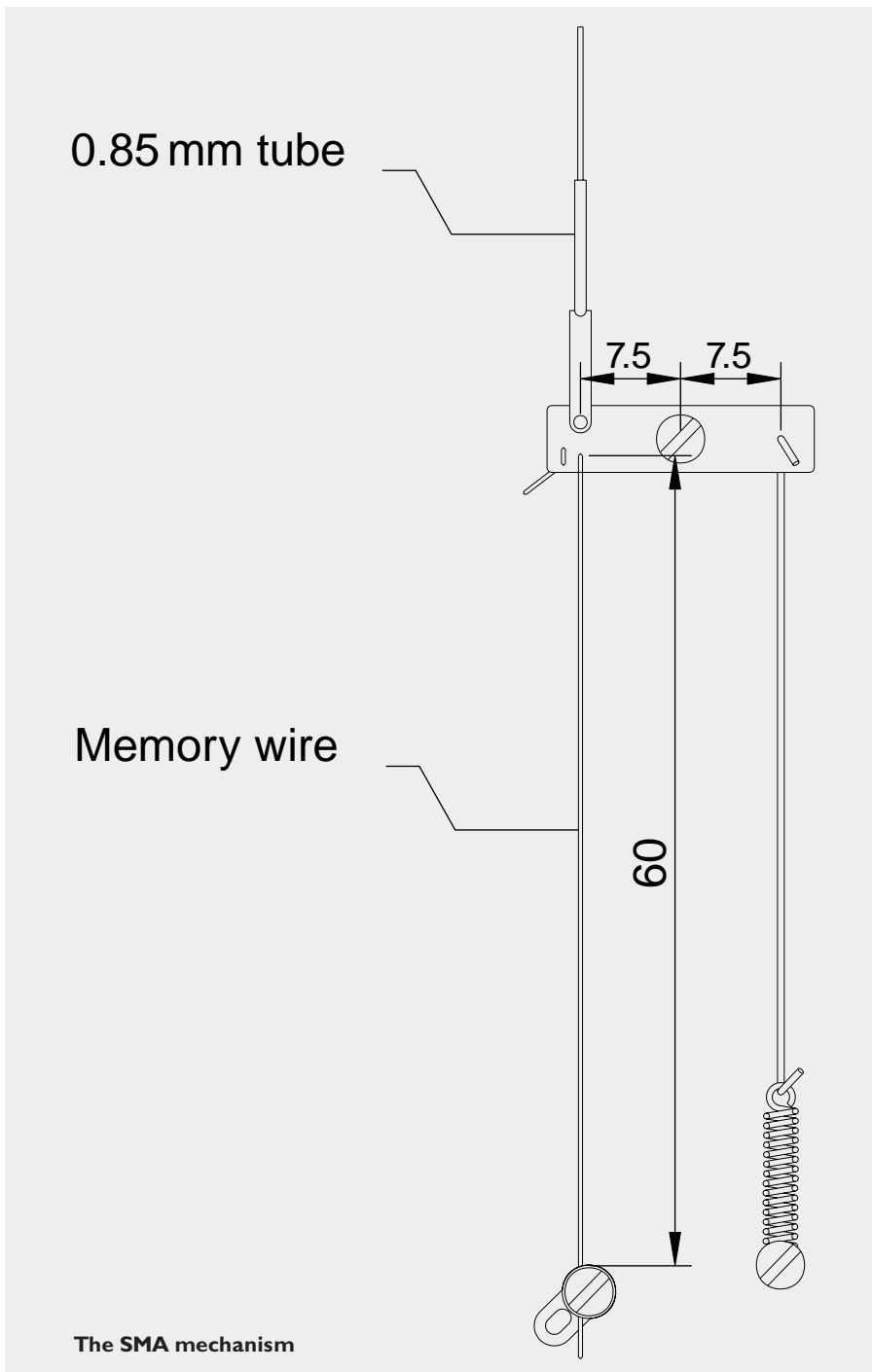
You can see in the photographs, that I have wired my signals through small sockets to make them easily removable. I have also set them up to run on a 12V supply, which requires the hefty 5W, 56 ohm resistor pictured. The resistor could be as small as 2W, but no smaller, as the current is quite high. The resistor value required for a given supply voltage, based on a device operating current of 200mA, is given by Ohm's law: $R = V/0.2$

When power is supplied to the mechanism, the memory wire contracts, pulling the signal arm on and extending the return spring. When the power is turned off, the wire cools and the spring contracts returning the signal to off. The action of these devices is silky smooth over a period of 1–2



Photographs and illustrations by Lawrence Boul





seconds. Hard to demonstrate in an article on the printed page!

SMA devices won't overcome flaws in the assembly of the signals, though. At a recent exhibition I had some minor operational problems with one of the signal arms on my layout. The arm concerned does not have the best range of movement, nor is it as free as it might be. Part of the problem was a bit of a technical hitch when painting that saw me freeze the mechanism. Also, as always when preparing for an exhibition, the darn things were only finished a day or two before the show, so we had no opportunity for proper testing or remedial action. The take home message for me is that one has to get these basics sorted out.

Sources

The memory wire (120 μm) and return springs used were from Jacques Le Plat at Pro-Rail International of Belgium. His introductory kit contains a useful booklet covering theory and practice.

Pro-Rail International

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Technical bit

Shape memory alloy is used for some very tricky purposes in medicine, aerospace and other high technology industries. Apparently the alloys have been woven into fabric to manufacture a shirt, the sleeves of

which automatically roll up when it gets warm. An Internet search will generate a mass of technical details and interesting reading.

For the purpose of signal operation a very fine wire is used which contracts when heated. This property is quite different from that involved in the 'hot wire' signal operation reported some years ago. That involved heating a nichrome wire to make it elongate. With nichrome, the resulting movement is continuous over a range of temperature, and is relatively small – necessitating a long wire. With SMA the movement is relatively large (3.5% with the material I use) and discrete. Which is to say it is either in the short or long condition (or in transition between the two with no over-run). This means that the length of the wire used determines the amount of movement, not the ambient or generated temperatures. The action is in many ways analogous to a muscle, and 'muscle wire' is the brand name of an SMA product marketed by Mondotronics.

Memory Wires are made from a nickel-titanium SMA. Such alloys have the ability to change their crystal structure according to temperature. At room temperature, their crystal mesh is of the martensitic type and it changes into the austenitic type at a pre-defined higher temperature. If an SMA sample is deformed at room temperature by stretching, this 'martensitic' deformation will be cancelled when passing to the austenitic structure and the sample will automatically return to its original shape. The alloy behaves as though it has recorded its original manufactured shape and keeps remembering it through subsequent deformations, hence the term 'Shape Memory Alloy'.

This memory effect is termed 'one-way' since the material only returns to one basic shape. To recycle the process, the sample must be put out of shape by an external force again. A 'two-way' effect can be obtained if the initial deformation is applied at the manufacturing stage so that it is recorded in the metal structure just like the basic undeformed shape. Now the sample not only returns to its basic shape when heated, but also goes back to its originally deformed shape when the temperature drops. In other words, the sample now oscillates between two specific shapes according to temperature. With two-way or reversing SMAs, an external deformation force is not necessary. The material behaves with a dual shape memory, altering shape with temperature alone.


Wire of 120 microns (0.12 mm diameter, or about the thickness of a hair) is convenient for most modelling applications. Such a wire requires a heating current of

approximately 200mA to fully contract. Required voltage can be determined experimentally, and will depend on the wire length. A good method is to connect the device to a model railway throttle and slowly increase the voltage, while measuring the current with a meter. At 220-230mA the wire will have contracted, and the appropriate operating voltage can be read from the meter. While 200 mA is enough to operate the wire unloaded, in

my experiments a bit extra was needed to operate a signal mechanism.

The Pro-Rail wire has been manufactured to offer repetitive contractions of 3.5% of its supplied length. Therefore, a 2 mm displacement will require a working wire length of $2\text{ mm} / 0.035 = 60\text{ mm}$. Or for a 5 mm displacement, a working wire length of $5\text{ mm} / 0.035 = 140\text{ mm}$. Slop in working linkages should be allowed for when calculating the wire length required. Typical

lengths for convenient modelling use lie between five and fifteen centimetres requiring a voltage in the area of one to three volts.

For long term reliability, heating currents should not exceed 270 mA and the load should be less than 200g (or two newtons). If higher loads are required, multiple wires can be used. High temperatures destroy the memory properties, and for this reason the wires should always be crimped or clamped and never soldered. 

Where was that loco?

Location of locomotives – South Island

Christchurch				Greymouth				Dunedin				Invercargill	
A	C	Ec	Rm	A	Ds	A	B	JA	A	DsA			
421	845	7	50	415	210	413	305	1249	71	250			
598	846	8	51	418	213	414	308	1250	161	251			
602	847	9	52	422	215	417		1251	178	252			
	848	10	53	423		426	BA	1252	406				
AB	849	11	54	424	Eo	470	497	1253	407	JA			
609	850	12	57	425	2		498	1255	411	1254			
612	863		58	428	3	AB	500	1256	416	1271			
615	864	F	108	471	4	608	551	1257	427	1272			
616	865	13	109	472	5	613	552	1258		1273			
617	866	163	110	474	6	658	554	1259	AB				
665	867		111	475		660		1260	719	TR			
688	868	JA	112	477	WA	663	DH	1261	721	64			
689		1240	113	478	137	690	758	1262	725	165			
692	Ds	1241	114	578	289	691	759	1263	726				
695	202	1242	115	580		693	766	1274	729	WF			
696	203	1243	126	581	WE	694	772		730	379			
697	204	1244	127		375	706	777	RM	731	382			
699	209	1245	134	AB	376	727	778	55	732	387			
704	211	1246		610	377	728	779	56	778	394			
718	212	1247	TR	722		746	780		784	402			
720	214	1248	18	723	WF	777	781	TR	*803	430			
724		1264	34	755	380	779	782	35	805	433			
740	DsA	1265	36	804	383	781	783	81	810	438			
750	256	1266	62	808	403	782		156		842			
762	257	1267	63	820		*788	DsA	164	Ds	844			
776	258	1268	153	823	Ww	*789	253	171	200				
780		1269	154		571	*791	254		201				
783	DsB	1270	155	B	573	*792	255	WF	205				
785	305			303	575	*793	259	391	206				
*786	306	KB	WF	304	644	*795	260						
*787	307	965	389	306	669	812	261	Ww					
*790	308	966	390	307	672	822	262	574					
798	309	967	393		678		263						
806	317	968	401	BA	679		264						
807		969	468	148	680								
809		970		499	683								
811				553	684								
813													
821													
833													

*WAB conversion

CLASS	A	AB	B	BA	C	DH	Ds	DsA	DsB	Ec	Eo	F	JA	KB	Rm	TR	WA	WE	WF	Ww	TOTAL
No	32	81	6	9	12	11	14	15	6	6	5	2	35	6	20	15	2	3	19	12	311

This table is transcribed from an official NZGR notice, dated 1962, in Colin Barry's collection.